

THE WATER ENVIRONMENT AND HUMAN NEEDS: A CASE STUDY INVOLVING THE HYDRODYNAMICS OF A COASTAL LAKE IN SOUTHERN CHILE

Yarko Niño Department of Civil Engineering, Universidad de Chile

THE WATER ENVIRONMENT AND HUMAN NEEDS

... THIS WIDER SCOPE OF APPROACHING FUTURE PROBLEMS OF THE WATER ENVIRONMENT ... WHEN ALL THE COMPLEX ENVIRONMENTAL AND SOCIAL FACTORS MUST BE CONSIDERED IN A GIVEN SYSTEM TO MEET THEM WITH CREATIVE IDEAS AND TECHNOLOGY AT PRESENT STILL LARGELY UNKNOWN ...

(A.T. IPPEN, 1970)

THE PLAN

→ EXPLORE A SYSTEM WHOSE HYDRODYNAMICS HAS A STRONG IMPACT ON THE ENVIRONMENT AND WELL-BEING OF LOCAL COMMUNITIES

➔ IN THE PROCESS DISCUSS ASPECTS OF TRANSPORT AND MIXING IN STRATIFIED FLOWS

→ GO FROM THEORY TO PRACTICE (THROUGH EXPERIMENTS AND NUMERICAL MODELING)

RIVER AND LAKE BUDI





38° 52` 73° 22`

SALINITY STRATIFICATION AND DISSOLVED OXYGEN



BUDI RIVER MOUTH (ICOL)



ARTIFICIAL OPENING



ARTIFICIAL OPENING



SOCIAL AND ENVIRONMENTAL ISSUES

→ LAKE BUDI IS LOCATED IN A REGION OF LOW-INCOME RURAL NATIVE PEOPLE (MAPUCHE) COMMUNITIES

➔ MAIN ECONOMIC ACTIVITIES ARE SMALL-SCALE FISHING AND AGRICULTURE

→ IN RECENT YEARS FISHING IN THE LAKE HAS DECLINED FORCING LAND-USE CHANGES FOR AGRICULTURE

→ THIS HAS FORCED EARLIER IN THE YEAR AND MORE FREQUENT OPENINGS OF THE MOUTH BAR AND DECAYING WATER QUALITY IN THE LAKE

FIELD OBSERVATIONS 2006-2007

→ 2 MOUTH-BAR OPENINGS IN THE AUSTRAL WINTER OF 2006: JUNE 22 AND OCTOBER 5

→ OCTOBER 2 (3 DAYS PRIOR 2ND OPENING)

→ OCTOBER 18 (2 WEEKS AFTER 2ND OPENING)

→ DECEMBER 12 (10 WEEKS AFTER 2ND OPENING)

→ JANUARY 29 (17 WEEKS AFTER 2ND OPENING)

SALINITY STRUCTURE PRIOR 2ND OPENING

OCTOBER 2



4 6 8 10 12 14 16 18 SALINITY (pss)

SALINITY STRUCTURE 2WEEKS POST 2ND OPENING

OCTOBER 18



SALINITY STRUCTURE 10 WEEKS POST 2ND OPENING

DECEMBER 18



SALINITY STRUCTURE 17 WEEKS POST 2ND OPENING

JANUARY 29 COMPLETE MIXING!









ELLISON & TURNER (1959)



$$\frac{\partial(U\ h)}{\partial t} + \frac{\partial(U^2\ h)}{\partial x} = S_1\ g\ B\ h\ S - \frac{1}{2}\ S_2\ g\ \frac{\partial(B\ h^2)}{\partial x} - c_f\ U^2$$

$$\frac{\partial Bh}{\partial t} + \frac{\partial (U \ B \ h)}{\partial x} = 0$$

ELLISON & TURNER (1959)

DENSITY CURRENT IN THE LAKE (2 WEEKS POST 2ND OPENING)





DAILY MEAN FLOW RATES



WIND MIXING IN TWO-LAYER FLUID



$$Ri_* = \frac{g (\rho_2 - \rho_1) / \rho_0 h_1}{u_*^2}$$
 WIND RICHARDSON NUMBER

EXPERIMENTS (NIÑO ET AL., 2003)

DENSITY MAPS, $Ri_* = 82.6$



EXPERIMENTS (NIÑO ET AL., 2003)

(KRANENBURG, 1985; MONISMITH, 1986)



LET'S DO SOME THEORY IPPEN'S STYLE (e.g., HARLEMAN & IPPEN, 1966)

BULK MIXING EFFICIENCY

$$\Gamma_{mix} = \frac{dPE/dt}{dK/dt}$$

(TSENG & FERZIGER, 1998)

 $\label{eq:GAIN IN PE} \begin{array}{c} \operatorname{GAIN} \operatorname{IN} \operatorname{PE} & \displaystyle \frac{d(PE/A)}{dt} = \frac{1}{2} \; g \; (\rho_2 - \rho_1) \; h_1 \; \frac{dh_1}{dt} \end{array}$

WIND INPUT

$$\frac{(K/A)}{dt} = \rho_0 \ u_*^2 \ u_s$$

 $k = \frac{u_s}{u_*}$ FRICTION FACTOR

$$\frac{u_e}{u_*} = 2 \ k \ \Gamma_{mix} \ \frac{1}{Ri_*}$$

 $\Gamma_{mix} \approx 0.0018$ (0.2%)

LET'S TRY A DIFFERENT APPROACH!

TKE BALANCE
$$\frac{DK}{Dt} = Diffusion + P + G - \epsilon$$

$$P + G - \epsilon = 0$$

MIXING EFFICIENCY

$$\gamma_{mix} = -\frac{G}{\epsilon} \approx 0.15 \text{ (WÜEST & LORKE, 2003)}$$

$$G = D_t \; (\frac{-g}{\overline{\rho}} \; \frac{\partial \overline{\rho}}{\partial z})$$

TURBULENT DIFFUSIVITY $D_t = \frac{\gamma_{mix} \epsilon}{N^2}$



$$\begin{split} \frac{\partial S}{\partial t} &= \frac{\partial}{\partial z} (D_t \; \frac{\partial S}{\partial z}) \\ \frac{\partial (h_1 S_1)}{\partial t} &= -(D_t \; \frac{\partial S}{\partial z})_{int} = S_2 \; u_e \end{split}$$

$$\begin{aligned} (\rho_2 - \rho_0) \ u_e &= -D_t \left(\frac{\partial \rho}{\partial z}\right)_{int} - \frac{\rho_0}{g} N^2 \\ \frac{\gamma_{mix} \ \epsilon}{N^2} \\ \\ \frac{u_e}{u_*} &= \gamma_{mix} \ \epsilon^* \ \frac{1}{Ri_*} \\ \end{aligned} \qquad \epsilon^* &= \frac{\epsilon \ h_1}{u_*^3} \quad \text{VALUE?} \end{aligned}$$

$\textit{K-} \mathcal{E} \text{ MODEL WITH BUOYANCY EFFECTS}$



K-E MODEL WITH BUOYANCY EFFECTS



$$\frac{u_e}{u_*} = \gamma_{mix} \ \epsilon^* \ \frac{1}{Ri_*}$$

 $\gamma_{mix} \ \epsilon^*|_{int} \approx 0.03 < 0.07$

ENTRAINMENT VELOCITY



ENTRAINMENT VELOCITY



 \rightarrow $u_{\rm e}/u_* \approx 2 \times 10^{-5}$ $Ri_* \approx 2.2 \times 10^4$





MIXING DUE TO BENTHIC BOUNDARY LAYER TURBULENCE

$$\epsilon^* \approx O(\frac{1}{\kappa}) \sim 2.5$$

MODELING SALINITY INTRUSION AND MIXING



MODELING DISSOLVED OXYGEN CONCENTRATION



PREDICTION IN THE CASE OF NATURAL MOUTH BAR OPENING



FINAL REMARKS

→ PRESENT MOUTH BAR MANAGEMENT WOULD NOT BE COMPATIBLE WITH FISH ECOLOGICAL DYNAMICS

→ BETTER PRACTICE MUST COMPATIBILIZE FLOODING PROTECTION, WATER QUALITY, LAKE ECOLOGY, AND LOCAL COMMUNITIES WELFARE

→ RESEARCH IS FUN BUT IS MORE FUN WHEN IT IS PUT AT THE SERVICE OF PROTECTING AND IMPROVING SOCIAL AND ENVIRONMENTAL CONDITIONS THANKS TO:

FELIPE SANDOVAL CLAUDIA RODRIGUEZ MANUEL CONTRERAS

TURBULENT INTENSITY PARAMETER (IVEY ET AL., 2008)

$$I = \frac{\epsilon}{\nu N^2} \qquad \qquad I = \frac{\epsilon}{\nu N^2} = \epsilon^* \frac{Re_*}{Ri_*} \frac{L_i}{h_1}$$
$$Re_* = \frac{u_* h_1}{\nu} \qquad \qquad \qquad L_i = \frac{\Delta \rho}{-(d\rho/dz)}$$

$$Re_* \approx 3 \times 10^4$$
LAKE BUDI
$$Ri_* \approx 2 \times 10^4 \quad \rightarrow \quad I \approx 0.15$$

$$L_i/h_1 \approx 0.2$$

EXPERIMENTS NIÑO ET AL. (2003): $I \approx$ 1-15 WUEST & LORKE (2005): $I \approx$ O(1) AT LAKES THERMOCLINE

TURBULENT INTENSITY PARAMETER (IVEY ET AL., 2008)

$$I = \frac{\epsilon}{\nu N^2}$$

I RANGE	REGIME	
l < 7	MOLECULAR	CHECK!
7< l < 100	TRANSITIONAL	
l > 100	ENERGETIC	

MIXING DUE TO BENTHIC BOUNDARY LAYER TURBULENCE

$$\epsilon^* \approx O(\frac{1}{\kappa}) \sim 2.5$$